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This is probably the most misused table in the Code book as the ampacities listed in Table 310.16 are generally never correct. This is a very important table that you must learn to use correctly.

Table 310.16. Allowable Ampacities of Insulated Conductors
Rated 0-2000 Volts, $60^{\circ}$ to $90^{\circ} \mathrm{C}\left(140^{\circ}\right.$ to $\left.194^{\circ} \mathrm{F}\right)$
Not More Than Three Conductors in Raceway or Cable or Earth
(Directly Buried), Based on Ambient Temperature of $30^{\circ} \mathrm{C}\left(86^{\circ} \mathrm{F}\right)^{*}$.

| Size | Temperature Rating of Conductor. See Table 310.4(A). |  |  |  |  |  | Size |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AWG <br> kemil | $\begin{gathered} 60^{\circ} \mathrm{C} \\ \left(140^{\circ} \mathrm{F}\right) \\ \hline \end{gathered}$ | $\begin{gathered} 75^{\circ} \mathrm{C} \\ \left(167^{\circ} \mathrm{F}\right) \end{gathered}$ | $\begin{gathered} 90^{\circ} \mathrm{C} \\ \left(194^{\circ} \mathrm{F}\right) \\ \hline \end{gathered}$ | $\begin{gathered} 60^{\circ} \mathrm{C} \\ \left(140^{\circ} \mathrm{F}\right) \end{gathered}$ | $\begin{gathered} 75^{\circ} \mathrm{C} \\ \left(167^{\circ} \mathrm{F}\right) \\ \hline \end{gathered}$ | $\begin{gathered} 90^{\circ} \mathrm{C} \\ \left(194^{\circ} \mathrm{F}\right) \end{gathered}$ | AWG <br> kemil |
| kemil | TYPES TW, UF | RHW, THHW, THW, THWN, XHHW, XHHWN, USE, ZW | TYPES TBS,SA, SIS, FEP, FEPB, MI, PFA RHH, RHW-2, THHN, THHW, THW-2, THWN-2 USE-2, XHH XHHW, XHHW-2 Z ZW-2 | $\begin{gathered} \text { TYPES } \\ \text { TW, } \\ \text { UF } \end{gathered}$ | RHW, THHW, THW, THWN, XHHW, USE | TYPES TBS, SA, SIS, THHN, THHW, THW-2, THWN-2, RHH, RHW-2, USE-2, XHH, XHHW, XHHW-2, XHHN | kemil |
|  | COPPER |  |  | ALUMINUM OR COPPER-CLAD ALUMINUM |  |  |  |
| 18** | $\ldots$ | .... | 14 | ... | $\ldots$ | . | . |
| 16** | $\ldots$ | $\ldots$ | 18 | $\ldots$ | .... | .... | $\ldots$ |
| 14** | 15 | 20 | 25 |  |  | .... |  |
| 12** | 20 | 25 | 30 | 15 | 20 | 25 | 12** |
| 10** | 30 | 35 | 40 | 25 | 30 | 35 | 10** |
| 8 | 40 | 50 | 55 | 35 | 40 | 45 | 8 |
| 6 | 55 | 65 | 75 | 40 | 50 | 55 | 6 |
| 4 | 70 | 85 | 95 | 55 | 65 | 75 | 4 |
| 3 | 85 | 100 | 115 | 65 | 75 | 85 | 3 |
| 2 | 95 | 115 | 130 | 75 | 90 | 100 | 2 |
| 1 | 110 | 130 | 145 | 85 | 100 | 115 | 1 |
| 1/0 | 125 | 150 | 170 | 100 | 120 | 135 | 1/0 |
| 2/0 | 145 | 175 | 195 | 115 | 135 | 150 | $2 / 0$ |
| 3/0 | 165 | 200 | 225 | 130 | 155 | 175 | $3 / 0$ |
| 4/0 | 195 | 230 | 260 | 150 | 180 | 205 | 4/0 |
| 250 | 215 | 255 | 290 | 170 | 205 | 230 | 250 |
| 300 | 240 | 285 | 320 | 195 | 230 | 260 | 300 |
| 350 | 260 | 310 | 350 | 210 | 250 | 280 | 350 |
| 400 | 280 | 335 | 380 | 225 | 270 | 305 | 400 |
| 500 | 320 | 380 | 430 | 260 | 310 | 350 | 500 |
| 600 | 350 | 420 | 475 | 285 | 340 | 385 | 600 |
| 700 | 385 | 460 | 520 | 315 | 375 | 425 | 700 |
| 750 | 400 | 475 | 535 | 320 | 385 | 435 | 750 |
| 800 | 410 | 490 | 555 | 330 | 395 | 445 | 800 |
| 900 | 435 | 520 | 585 | 355 | 425 | 480 | 900 |
| 1000 | 455 | 545 | 615 | 375 | 445 | 500 | 1000 |
| 1250 | 495 | 590 | 665 | 405 | 485 | 545 | 1250 |
| 1500 | 525 | 625 | 705 | 435 | 520 | 585 | 1500 |
| 1750 | 545 | 650 | 735 | 455 | 545 | 615 | 1750 |
| 2000 | 555 | 665 | 750 | 470 | 560 | 630 | 2000 |

*Table 310.15(B)(1) CORRECTION FACTORS based on $30^{\circ} \mathrm{C}\left(86^{\circ} \mathrm{F}\right)$

| Ambient | For ambient temperatures other than $30^{\circ} \mathrm{C}\left(86^{\circ} \mathrm{F}\right)$, multiply the ampacities shown above by the appropritate factor shown below. |  |  |  |  |  | Ambient |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 or less | 1.29 | 1.20 | 1.15 | 1.29 | 1.20 | 1.15 | 50 or less |
| 11-15 | 1.22 | 1.15 | 1.12 | 1.22 | 1.15 | 1.12 | 51-59 |
| 16-20 | 1.15 | 1.11 | 1.08 | 1.15 | 1.11 | 1.08 | 60-68 |
| 21-25 | 1.08 | 1.05 | 1.04 | 1.08 | 1.05 | 1.04 | 69-77 |
| 26-30 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 78-86 |
| 31-35 | . 91 | . 94 | . 96 | . 91 | . 94 | . 96 | 87-95 |
| 36-40 | . 82 | . 88 | . 91 | . 82 | . 88 | . 91 | 96-104 |
| 41-45 | . 71 | . 82 | . 87 | . 71 | . 82 | . 87 | 105-113 |
| 46-50 | . 58 | . 75 | . 82 | . 58 | . 75 | . 82 | 114-122 |
| 51-55 | . 41 | . 67 | . 76 | . 41 | . 67 | . 76 | 123-131 |
| 56-60 |  | . 58 | . 71 |  | . 58 | . 71 | 132-140 |
| 61-65 | - | . 47 | . 65 | - | . 47 | . 65 | 141-149 |
| 66-70 | - | . 33 | . 58 | - | . 33 | . 58 | 150-158 |
| 71-75 | - | - | . 50 | - | - | . 50 | 159-167 |
| 76-80 | - | - | . 41. | - | - | . 41. | 168-176 |
| 81-85 |  |  | 29 |  | - | 29 | 177-185 |

[^0]The reason for the misuse of the table comes from not reading the heading which states the ampacities shown for the various conductors are correct if you don't: (1) install over three current carrying conductors in a raceway or cable (2) exceed $30^{\circ} \mathrm{C}$ or $86^{\circ} \mathrm{F}$ in ambient temperature.

$60^{\circ}$ to $90^{\circ} \mathrm{C}\left(140^{\circ}\right.$ to $\left.194^{\circ} \mathrm{F}\right)$ Not more Than Three Conductors in Raceway or Cable or Earth (Directly Buried), Based on Ambient Air Temperature of $30^{\circ} \mathrm{C}\left(86^{\circ} \mathrm{F}\right)$.


Common sense would remind you that normally you are installing more than three conductors in a conduit and also the surrounding temperature of these conductors would be above $86^{\circ} \mathrm{F}$. The normal ampacities listed in the table must be corrected if either condition (1) or (2) is present.

The conductor ampacity is the current carried continuously without increasing the temperature of its insulation beyond the danger point. The conductor ampacity varies with the type of insulation and the method of installation.


Except for mechanical abuse, the greatest hazard that conductors must endure is heat. Conductor insulation can be damaged by excessive heat in various ways, depending on the type of insulation and the degree of overheating. Continued exposure to excessive heat causes insulation to become soft, perhaps to melt, and in extreme cases to burn.

This heat comes from two sources: From the ambient air surrounding the conductors or from the current the conductors must carry. There is a point where an increase in current causes excessive heat even though conducting materials such as copper or aluminum have a low resistivity.

For many years natural rubber was used to insulate conductors, but age along with heat caused such rubber insulation to dry out, to crack, and to become brittle. Today we have better quality rubber and thermoplastic materials that not only permit thinner insulation on conductors but also withstand temperature better resulting in higher ampacities of conductors.

The maximum temperature permitted for conductor insulation is called the temperature rating of the conductor. Table $\mathbf{3 1 0 . 4 ( A )}$ shows the maximum temperature that the insulation type is permitted to reach. That maximum temperature will be reached when a conductor is loaded to its full ampacity in an ambient temperature of 30 degrees C or 86 degrees F .

The type letter on the insulation indicates its insulation, maximum operating temperature, and application provisions.

RHW insulation, the " R " indicates rubber insulation. The " H " indicates $75^{\circ} \mathrm{C}-167^{\circ} \mathrm{F}$ maximum operating temperature (insulation rating). The " W " indicates moisture resistant.

THHN insulation, the " T " indicates thermoplastic insulation. The "HH" indicates $90^{\circ} \mathrm{C}-194^{\circ} \mathrm{F}$ maximum operating temperature (insulation rating). The " N " indicates nylon covering.


The \#10 THW has a maximum operating temperature of $75^{\circ} \mathrm{C}$ which is $167^{\circ} \mathrm{F}$.


The \#10 THHN has a maximum operating temperature of $90^{\circ} \mathrm{C}$ which is $194^{\circ} \mathrm{F}$. An " HH " rated insulation will allow more heat to be dissipated faster than an " H " rated insulation thus raising the ampacity (the current the conductor can carry safely without damage).

The maximum operating temperature is the insulation rating of the conductor and must not be exceeded. Proper designing is a very important factor.

You must first understand what words mean; such as ampacity, ambient temperature, insulation rating, etc.


A \#10 TW conductor has an ampacity of 30 amperes. The insulation rating is $60^{\circ} \mathrm{C}$ or $140^{\circ} \mathrm{F}$.
This does not mean that a TW insulation can be installed where the ambient temperature reaches $140^{\circ} \mathrm{F}$.

What this means is: If a \#10 TW conductor is loaded to the allowable ampacity, 30 amperes in an ambient that has a temperature of $30^{\circ} \mathrm{C}$ or $86^{\circ} \mathrm{F}$, the temperature of the insulation will reach $60^{\circ} \mathrm{C}$ or $140^{\circ} \mathrm{F}$.

Table 310.16 the table of ampacity is aimed at designating a level of current that will permit the conductor to reach its thermal limit, but not exceed it.


\#10 TW 30 amps of current flowing

The 30 amps of current flowing produces heat in the conductor which must dissipate through the insulation to the ambient.

With the ambient temperature at $86^{\circ} \mathrm{F}$ and with 30 amperes of current flowing through the conductor, a thermometer placed on the insulation would read $140^{\circ} \mathrm{F}$ which is maximum operating temperature for this type insulation (TW).


For a \#10 TW conductor, any current above 30 amps or any ambient temperature above $86^{\circ} \mathrm{F}$ will cause insulation damage, as you will exceed the maximum operating temperature of the conductor; $140^{\circ} \mathrm{F}$.

Maximum operating temperature $=$ Full ampacity at $86^{\circ} \mathrm{F}$.
$140^{\circ} \mathrm{F}-86^{\circ} \mathrm{F}=54^{\circ} \mathrm{F}$ for the 30 amperes of current flow in the \#10 TW conductor.


## ADJUSTMENT FACTORS



When there are more than three current-carrying conductors in a raceway or cable, the ampacity of each conductor must be reduced as indicated in Table 310.15(C)(1) to compensate for heating effects and reduced heat dissipation due to reduced ventilation of individual conductors.

Table 310.15(B)(3)(a). Adjustment Factors.
(a) More than Three Current Carrying Conductors in a Raceway or Cable. Where the number of conductors in a raceway or cable exceeds three, the ampacities shall be reduced as shown in the following table:

|  | Percent of Values in Tables 310.16 through Table <br> 310.19 as Adjusted for Ambient Temperature if |
| :---: | :---: |
| Number of | Necessary |
| Conductors | 80 |
| 4 through 6 | 70 |
| 7 through 9 | 50 |
| 10 through 20 | 45 |
| 21 through 30 | 40 |
| 31 through 40 | 35 |
| 41 and above |  |

Example: A conduit contains six \#8 TW current carrying conductors. The normal ampacity is 40 amps $x 80 \%$ from Table $310.15(B)(3)(a)=32$. The maximum current that can be passed through the \#8 TW conductor without subjecting it to insulation damage is 32 amps .

Adjustment factors also apply when paralleling conductors per Section 310.10(H)(4).


It is wrong to think since you connected two conductors in parallel on one lug that you now only have one conductor. Heat is measured by $\mathrm{W}=I^{2}$. In parallel you have two conductors carrying current producing heat.


It is wrong to think that by using a larger size conduit than required would satisfy the adjustment factor required for the reduction of ampacity. The larger conduit would have more volume area, but it's like heating a rock, it may take a little longer but it will still reach the same temperature.


To avoid applying the adjustment factors of $310.15(\mathrm{C})(1)$ you can install two separate conduits as shown below. Now you only have 3 current carrying conductors in each conduit.


Some conductors are not counted when applying 310.15(C)(1):

| $310.15(\mathrm{C})(1)$ | Conductors of different systems |
| :--- | :--- |
| $310.15(\mathrm{C})(2)$ | Cable trays |
| $310.15(\mathrm{C})(1)(\mathrm{b})$ | Nipples |
| $310.15(\mathrm{C})(1)(\mathrm{c})$ | Outdoor trench |
| $310.15(\mathrm{E})(1)$ | The neutral conductor in a normally balanced circuit is not counted |

But, 310.15(E)(2) states: The neutral conductor is counted in a 3-wire circuit consisting of 2-phase wires of a 3-phase wye system.
310.15(E)(3) states: The neutral is considered a current carrying conductor in nonlinear loads. Circuits such as discharge lighting (fluorescent, mercury, sodium) data processing, or similar equipment. The Harmonic currents in the nonlinear loads can cause the neutral currents to rise a little higher than the line current.
310.15(F) states: A grounding or bonding conductor shall not be counted when applying the provisions of Table $310.15(\mathrm{C})(1)$ The grounding conductor (green or bare wire) only carries fault current to trip the overcurrent device. This is not a heat factor.


Summary of $310.15(\mathrm{C})(1)$ on when to count the neutral as current carrying:


Non-linear loads which contain harmonic currents


When a linear load is turned on, the voltage and current start and turn off together. When a nonlinear load is turned on, the voltage starts but the current is purposely delayed.

Harmonic simply indicates that the current waveform is distorted. The closer the waveform is to a fundamental sine wave, the lower the harmonic content. With a fundamental sine wave, there are no high order harmonics.

A 3rd harmonic makes 3 alternations in one alternation of the fundamental wave form. A 5th harmonic makes 5 alternations in one alternation of the fundamental wave. The 7th harmonic makes 7 alternations, and so on.


The highest peak of the wave is determined by adding all of the odd harmonics together. The frequency is determined by the number of complete cycles per second, measured in Hertz. 60 cycles per second equals 60 Hertz , or 60 Hz .

On a 60 Hz AC system, the 3 rd harmonic is 180 Hz , the 5 th harmonic is 300 Hz , the 7th harmonic is 420 Hz , etc.



A harmonic wave is a distorted wave pattern consisting of the fundamental wave and other higher frequency waves that are superimposed on the fundamental wave.

The harmonic currents are delayed then added together and then burst into action causing a high peak wave form and a higher frequency.


Heat is increased by an increase in current frequency. The heating effect on transformers, circuit breakers and conductors supplying non-linear loads is a function of $\mathbf{I}^{2} \mathbf{R}$.

The higher $I^{2} R$ heating where harmonic currents are supplied is caused by what is known as skin effect. Skin effect is an increase in resistance due to the fact that higher-frequency currents flow on the skin of the conductor, rather than throughout the entire conductor.

AC tends to flow along the surface of a conductor. DC acts through the entire cross-sectional area of the conductor in a uniform manner. The name skin effect is given to the action whereby AC is forced toward the surface of the conductor. Because of skin effect, there is less useful copper conductive area with AC. As a result, there is an increase in resistance.

CROSS-SECTIONAL AREA DENSITY


For the 3 rd harmonic, instead of 60 Hz , it's now 180 Hz , there is a $42 \%$ change in the skin effect concentration point. For the 5th harmonic, there is a $55 \%$ difference and a $62 \%$ difference for the 7th harmonic. The result is a proportionate increase of resistance.

# CHAPTER 8 

| ExAM SPoNSOR |  |  | APPLICANT NUMBER |  |  | GRADE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Number |  |
| dATE $\qquad$ type exam - |  |  |  | (1) 0 | 00 |  |
|  |  | PaRt | (1)(1) (1) | (1) (1) | (1) (1) (1) |  |
|  |  |  | (2) (2) (2) | (2) 2 (2) | (2) (2) (2) |  |
| SAMPLE | W\%onc ${ }^{\text {Wen }}$ | MPOATANT IIIECTIOS F For | (3) 3 (3) | (3)3 | (3)3 3 3 |  |
| the neutral is | woing |  | (4) (4) 4 | (4) (4) 4 | (4)(4) (4) (4) |  |
| A) redin color | Whence |  | (5) (5) 5 | (5) 55 (5) | (5) 5 (5) 5 |  |
|  | Onco | - Enase | 6 6 6 | (6) 6 | (6) 6 6 |  |
| D) white in ocoror | ${ }^{\circ}$ |  | (7) 7 (7) | (7) 7 | (7) 778 |  |
|  |  | Mremer mer | (8)8 8 | (8)(8) | (8)8 88 |  |
|  |  |  | (9)(9) | (9) | (9999 |  |
| $\begin{aligned} & \text { ABBCD } \\ & \text { OOOO } \end{aligned}$ | 21 ABOCD | ${ }_{41} \mathrm{ABO} \mathrm{OB} \mathrm{D}$ | $\text { 〒 } \mathrm{ABOCD}$ |  | $\begin{aligned} & \text { AB B C } \\ & \text { OOD } \end{aligned}$ | $101 \text { ABOOD }$ |
| A B C D | ${ }^{\text {A B C D }}$ | $A \mathrm{BCD}$ | ${ }^{\text {A B C D }}$ |  | ${ }^{\text {A B C D }}$ | $A B C D$ |
| OOOO | 2 OOOO | 4 OOOO | $\checkmark 20000$ |  | 0000 | 1020000 |
| ${ }^{3} \mathrm{ABOCD}$ |  | $4{ }^{4} \mathrm{ABOCD}$ | ${ }_{63}{ }^{\text {A B B Cob }}$ |  |  |  |
| $A B C D$ | A B C D | A B C D | A B C D |  | A B C D | $A B C D$ |
| OOOO | 240000 | 40000 | ${ }^{64} 0000$ |  | 0000 | 1040000 |
| $\mathrm{ABOCO}^{\text {O }} \mathrm{O}$ | ${ }^{2}{ }^{\text {A }} \mathrm{OBOCD}$ | ${ }_{45}{ }^{\text {A OBOCO}}$ |  |  | AOBCD |  |
| $A B C D$ | $A \mathrm{BCD}$ | $A B C D$ | $A \mathrm{BCD}$ |  | A BCD | $A B C D$ |
| OOOO | ${ }^{26} 0000$ | 4 OOOO | ¢ OOOO |  | 0000 | 106 OOOO |
| ${ }^{\text {A B B }} \mathrm{O} \mathrm{CD}$ | ${ }^{27}{ }^{\text {A B B }} \mathrm{O} \mathrm{CD}$ | ${ }^{\text {A }} \mathrm{O} \mathrm{B} \mathrm{C}$ | ${ }^{\text {A B }} \mathrm{O} \mathrm{OCD}$ |  | ${ }^{\text {A B B Cob }}$ | $107{ }^{\text {A B B Cob }}$ |
| $A B C D$ | $A B C D$ | A ${ }^{\text {B }}$ | $A B C D$ |  | A ${ }^{\text {b }}$ | $A B C D$ |
| 0000 | ${ }^{28} 0000$ | 0000 | ${ }^{6} \mathrm{OOOO}$ |  | 0000 | 108000 |
| ${ }^{\text {A B B C }}$ | ${ }^{2} \mathrm{ABCD}$ | ${ }^{\text {A B C }}$ c ${ }^{\text {d }}$ | ${ }^{\text {A B C }}{ }^{\text {d }}$ |  | ${ }^{\text {A B C }}$ ¢ ${ }^{\text {d }}$ | 109000 |
| A BCD | ${ }^{2} \mathrm{OABCD}$ | $4{ }^{4} \mathrm{ABCD}$ | ${ }^{9} \mathrm{ABCOD}$ |  | A BCD | $109{ }^{1}$ |
| 10 OOOO | 3000 | so OOOO | \% OOOO |  | OOOO | 110 OOOO |
| ${ }^{\text {A B B }}{ }^{\text {d }}$ | ${ }^{\text {A }}{ }^{\text {B }} \mathrm{C}^{\text {D D }}$ | ${ }^{\text {A B }}{ }^{\text {c }}{ }^{\text {D }}$ | ${ }^{\text {A B C }}{ }^{\text {c }}$ |  | ${ }^{\text {A B C }}{ }^{\text {d }}$ | ${ }^{11}{ }^{\text {A }}{ }^{\text {B C }}{ }^{\text {d }}$ |
| ${ }^{11} \mathrm{OOBCO}$ | ${ }^{3} \mathrm{OOBCO}$ | ${ }^{51} \mathrm{OOBCO}$ | ${ }^{7} \mathrm{O} \mathrm{OBBCD}^{\text {a }}$ |  |  | ${ }^{111} \mathrm{OOCOO}$ |
| 12 OOOO | 32 OOOO | 52 OOOO | 7 OOOO |  | OOOO | 112 OOOO |
| ${ }^{13}{ }^{\text {A B B }} \mathrm{C}^{\text {D }}$ | ${ }^{3}{ }^{\text {A B B C D }}$ | ${ }^{\text {A B B }} \mathrm{C}^{\text {d }}$ | ${ }^{\text {A B C C D }}$ |  | ${ }^{\text {A B B }}{ }^{\text {c }}$ | ${ }_{13}{ }^{\text {A }}{ }^{\text {B }}{ }^{\text {c }}{ }^{\text {D }}$ |
| ${ }^{13} \mathrm{O} \mathrm{O} \mathrm{OOCO}$ | ${ }^{33} \mathrm{OOOOO}$ | O ${ }_{\text {a }}$ | ${ }^{73} \mathrm{O} \mathrm{OBOC}$ |  | O ${ }_{\text {a }}$ | ${ }^{113} \mathrm{O} \mathrm{O} \mathrm{OOCO}$ |
| 14 OOOO | ${ }^{34} 0000$ | 54 OOOO | ${ }^{74} \mathrm{OOOO}$ |  | 0000 | 1140000 |
| 15 A B ${ }^{\text {B }}$ | ${ }_{35}{ }^{\text {A B B C D }}$ | ${ }^{\text {A B }} \mathrm{C}$ | 75 ${ }^{\text {A B B }} \mathrm{O}$ |  | ${ }^{\text {A B C Cob }}$ |  |
|  | ${ }^{5} \mathrm{ABCD}$ |  |  |  | A B C D | W, ${ }_{\text {A B C D }}$ |
| ${ }^{16} \mathrm{OOOO}$ | ${ }^{3} \mathrm{OOOO}$ | s 0000 | ${ }^{7} \mathrm{OOOO}$ |  | 0000 | ${ }^{116} \mathrm{OOOO}$ |
|  | ${ }^{7}{ }^{\text {A B B }} \mathrm{O} \mathrm{CD}$ | $\checkmark{ }^{\text {a }} \mathrm{O} \mathrm{OBOD}$ | $\pi \mathrm{OBO}^{\mathrm{A}} \mathrm{O} \mathrm{C}$ |  | ${ }^{\text {A B B Cob }}$ |  |
|  | ABCD | ABCD |  |  | A BCD | $A{ }_{\text {A C }}$ D |
| ${ }^{18} \mathrm{OOOO}$ | ${ }^{3} \mathrm{OOOO}$ | ${ }^{58} \mathrm{OOOO}$ | ${ }^{78} \mathrm{OOOO}$ |  | OOOO | ${ }^{118} \mathrm{OOOO}$ |
| ${ }^{\text {A }}{ }^{\text {B C }} \mathrm{Cb}^{\text {d }}$ | ${ }^{\text {A B }} \mathrm{C}$ D | ${ }^{\text {A B }} \mathrm{C}^{\text {d }}$ |  |  | ${ }^{\text {A B C C }}$ | ${ }^{\text {A B C }}$ C ${ }^{\text {d }}$ |
| ${ }^{19} \mathrm{OOOO}$ | ${ }^{3} \mathrm{OOOO}$ | ${ }^{98} \mathrm{OOOO}$ | ${ }^{79} \mathrm{OOOO}$ |  | 0000 | 1190000 |
| ${ }^{20} \mathrm{O}^{\mathrm{A}} \mathrm{~B} \mathrm{CO} \mathrm{D}$ | ${ }^{40}{ }^{\text {A B O Cob }}$ |  | $\text { so } \stackrel{A}{\mathrm{O}} \mathrm{~B} \mathrm{~B} \mathrm{C} \mathrm{O} \mathrm{D}$ |  | AOBCD | ${ }_{120}^{120 \text { OBCOD }}$ |



Chapter 8 is a series of full calculation exams. The first exams are for the Journeyman Electrician level, the remaining exams are for the Master Electrician level.

Each exam contains 30 open book calculation questions with a time limit of three hours.
After completing each exam, turn to the answer sheets in the back of this book and grade yourself. $75 \%$ is passing.

To calculate your grade, simply divide the number of correct answers by the total number of questions (30). Example: 23 correct answers divided by 30 questions would equal $76.66 \%$.

Don't forget Tom Henry has 12 VIDEOS that cover all the chapters in this book and more!



[^0]:    * Refer to $310.15(\mathrm{~B})(1)$ for the amapacity correction factors where the ambient temperature is other than $30^{\circ} \mathrm{C}\left(86^{\circ} \mathrm{F}\right)$. Refer to 310.15(C)(1)(a) for more than three current carrying conductors.
    ** See Section 240.4(D)

